



APPLICATION FOR UNITED STATES PATENT

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Invention: LUBRICANTS

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LUBRICANTS

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The present invention relates generally to lubricants and more particularly to working fluid compositions contained in heat transfer devices which comprise the lubricant and a heat transfer fluid.

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Heat transfer devices of the mechanical compression type such as those used in refrigerators, freezers, heat pumps and automobile air conditioning systems are well known. In such devices a heat transfer fluid of a suitable boiling point evaporates at low pressure taking heat from a surrounding zone. The resulting vapour is then compressed and passes to a condenser where it condenses and gives off heat to a second zone. The condensate is then returned through an expansion valve to the evaporator so completing the cycle. The mechanical energy required for compressing the vapour and pumping the fluid is provided by, for example, an electric motor or an internal combustion engine.

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The heat transfer fluids used in these heat transfer devices include chlorine containing fluoroalkanes such as dichlorodifluoromethane (R-12), chlorodifluoromethane (R-22) and mixtures thereof with, for example, fluoroalkanes such as 1,1-difluoroethane (R-152a). However, such chlorine containing fluoroalkanes have been implicated in the destruction of the ozone layer and as a result the use and production thereof is to be severely limited by international agreement. The use of certain fluoroalkanes and hydrofluoroalkanes in place of the chlorine containing fluoroalkanes has been proposed. The fluoroalkanes and hydrofluoroalkanes of particular interest are those compounds which have comparable

5 boiling points and other thermal properties to the chlorine containing fluoroalkanes which they are replacing, but which are also less damaging or benign to the ozone layer. Thus, R-12 is generally being replaced by a new refrigerant, 1,1,1,2-tetrafluoroethane (R-134a).

10 Hitherto, heat transfer devices have tended to use mineral oils as lubricants. The good solubility of chlorine containing fluoroalkanes with mineral oils allows the mineral oil to circulate around the heat transfer device together with the chlorine containing fluoroalkane, and this in turn ensures proper
15 lubrication of the compressor. Unfortunately, however, the replacement fluoroalkane and hydrofluoroalkane heat transfer fluids such as R-134a have different solubility characteristics to the chlorine containing fluoroalkanes presently in use and tend to be
20 insufficiently soluble in mineral oils to allow the latter to be used as lubricants. Consequently, numerous alternative lubricants such as polyoxyalkylene glycols terminating in hydroxyl and other groups, esters of polyols with mono- and polyfunctional acids, and halo substituted esters and ethers have been proposed as
25 lubricants for use with the replacement heat transfer fluids.

30 Unfortunately, R-134a cannot be used as a direct replacement for certain of the refrigerants which are presently in use such as R-22 and R-502 (an azeotropic mixture of R-22 and chloropentafluoroethane R-115) since it does not possess comparable boiling characteristics and thermal properties. It has thus
35 been proposed that existing refrigerants such as R-22 and R-502 be replaced by refrigerant mixtures comprising two or more refrigerants selected from the

5 fluoroalkanes and hydrofluoroalkanes. Particular
mention may be made of binary mixtures of refrigerants
such as R-134a and difluoromethane (R-32) or R-32 and
pentafluoroethane (R-125). Unfortunately, these
refrigerant mixtures are also not sufficiently soluble
10 in mineral oils to allow the latter to be used as
lubricants. Moreover, the miscibility and solubility of
an alternative lubricant with one component of the
mixture, for example with R-134a, does not mean that
such a lubricant will also be miscible and soluble with
the refrigerant mixture itself. In consequence, the
15 development of a lubricant which exhibits acceptable
lubricating properties in a heat transfer device
utilising a refrigerant mixture presents a very real
problem.

It has now been found that if a prospective
20 lubricant is at least partially soluble in each
component of the refrigerant mixture then it will be at
least partially soluble in the refrigerant mixture
itself, thereby enabling its use as a lubricant with
that mixture. Such a lubricant may provide an
acceptable lubricating action even if it is immiscible
25 with one or more of the components of the refrigerant
mixture or with the refrigerant mixture itself.

According to the present invention there is
provided a working fluid composition comprising
(A) a heat transfer fluid comprising a mixture of at
30 least two compounds selected from the group consisting
of hydrofluoroalkanes and fluoroalkanes; and
(B) sufficient to provide lubrication of a lubricant
which is at least partially soluble in each component
of the heat transfer fluid.

35 The heat transfer fluid may comprise two, three or
more components. Preferred hydrofluoroalkanes and

5 fluoroalkanes are selected from the group consisting of difluoromethane (R-32), 1,1,2,2-tetrafluoroethane (R-134), 1,1,1,2-tetrafluoroethane (R-134a), pentafluoroethane (R-125), 1,1-difluoroethane (R-152a), 1,1,1-trifluoroethane (R-143a) and 1,1,2-trifluoroethane (R-143).

10 One suitable heat transfer fluid comprises a mixture of R-32 and R-125. Such a mixture may comprise equal proportions of each component on a weight basis.

15 The present invention is particularly concerned with the provision of a working fluid composition which provides a useful replacement for the working fluids presently in use which comprise R-22 or R-502 as the refrigerant and a mineral oil lubricant. A particularly desirable working fluid composition in this respect is one which comprises

20 (A) a heat transfer fluid comprising a mixture of:

- (1) tetrafluoroethane;
- (2) at least one hydrofluoroalkane selected from the group consisting of difluoromethane (R-32) and 1,1,1-trifluoroethane (R-143a); and optionally
- (3) pentafluoroethane (R-125); and

25 (B) sufficient to provide lubrication of a lubricant which is at least partially soluble in each component of the heat transfer fluid.

30 The tetrafluoroethane may be 1,1,1,2-tetrafluoroethane (R-134a) or 1,1,2,2-tetrafluoroethane (R-134) or a mixture of these two isomers. Preferably, however, the tetrafluoroethane is a single isomer, and more preferably is R-134a.

35 Although the heat transfer fluid may comprise more than three components, it is preferably a binary or ternary mixture. The mixture may be an azeotrope or near-azeotrope, but will normally be zeotropic.

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5 In one preferred embodiment of the present invention, the heat transfer fluid is a binary mixture consisting essentially of R-134a and R-32. Such a mixture provides a particularly suitable replacement for the R-22 refrigerant which has been used hitherto in commercial refrigeration systems and related heat transfer devices. Preferably, such a mixture comprises 10 from 45 to 75 % by weight, more preferably from 65 to 75 % by weight of R-134a and from 25 to 55 % by weight, more preferably from 25 to 35 % by weight of R-32. A particularly preferred binary mixture comprises about 15 70 % by weight of R-134a and about 30 % by weight of R-32.

In a further preferred embodiment of the present invention, the heat transfer fluid comprises a ternary or higher mixture of:

- 20 (1) R-134a or R-134;
(2) at least one hydrofluoroalkane selected from the group consisting of R-32 and R-143a; and optionally
(3) R-125.

25 Such a heat transfer fluid provides a suitable replacement for the R-22 and R-502 refrigerants which have been used hitherto in commercial refrigeration systems and related heat transfer devices.

Particularly suitable ternary heat transfer fluids may be selected from:

- 30 (a) R-134a + R-32 + R-143a;
(b) R-134 + R-32 + R-143a;
(c) R-134a + R-32 + R-125;
(d) R-134 + R-32 + R-125;
(e) R-134a + R-143a + R-125; and
(f) R-134 + R-143a + R-125.

35 A particularly preferred heat transfer fluid comprises a mixture of:

- 5 (1) R-134a or R-134, especially R-134a;
(2) R-32 or R-143a, especially R-32; and
(3) R-125.

Such heat transfer fluids provide a particularly suitable replacement for R-22 and R-502.

10 One particularly preferred ternary heat transfer fluid for replacing R-22 is a mixture consisting of:

- (1) 55 to 65 % by weight, particularly about 60 % by weight of R-134a;
(2) 25 to 35 % by weight, particularly about 30 % by weight of R-32; and
15 (3) 5 to 15 % by weight, particularly about 10 % by weight of R-125.

Another particularly preferred ternary heat transfer fluid for replacing R-22 is a mixture consisting of:

- 20 (1) 25 to 35 % by weight, particularly about 30 % by weight of R-134a;
(2) 45 to 55 % by weight, particularly about 50 % by weight of R-32; and
(3) 15 to 25 % by weight, particularly about 20 % by weight of R-125.

25 One particularly preferred ternary heat transfer fluid for replacing R-502 is a mixture consisting of:

- (1) 45 to 55 % by weight, particularly about 50 % by weight of R-134a;
30 (2) 25 to 35 % by weight, particularly about 30 % by weight of R-32; and
(3) 15 to 25 % by weight, particularly about 20 % by weight of R-125.

35 Another particularly preferred ternary heat transfer fluid for replacing R-502 is a mixture consisting of:

(1) 45 to 55 % by weight, particularly about 50 %
by weight of R-134a;

(2) 35 to 45 % by weight, particularly about 40 %
by weight of R-32; and

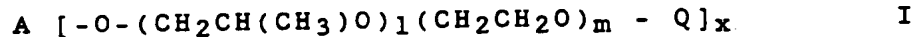
(3) 5 to 15 % by weight, particularly about 10 %
by weight of R-125.

All the percentages by weight quoted above are
based on the total weight of the ternary heat transfer
fluid.

Suitable lubricants may be selected from those
currently used with R-134a provided that the
requirement of partial solubility is met.

Lubricants satisfying the requirement of partial
solubility may, in particular, be selected from the
class known in the art as polyoxyalkylene glycols.
Suitable polyoxyalkylene glycol lubricants include
hydroxyl group initiated polyoxyalkylene glycols, e.g.
ethylene and/or propylene oxide oligomers/polymers
initiated on mono- or polyhydric alcohols such as
methanol, butanol, pentaerythritol and glycerol. Such
polyoxyalkylene glycols may also be end-capped with
suitable terminal groups such as alkyl, e.g. methyl
groups.

A preferred polyoxyalkylene glycol lubricant is
one having an average molecular weight in the range of
from about 150 to about 3000 and comprising one or more
compounds of general formula:



wherein

5 A is the residue remaining after removing the hydroxyl groups from a hydroxyl containing organic compound;

Q represents an optionally substituted alkyl, aralkyl or aryl group;

1 and m are independently 0 or an integer provided that at least one of l or m is an integer; and

30 x is an integer.

The polyoxyalkylene glycol lubricant may be prepared using conventional techniques. Such techniques are well known to those skilled in the art. Thus, in one method a hydroxyl containing organic compound such as an alcohol is reacted with ethylene oxide and/or propylene oxide to form an ethylene oxide and/or propylene oxide oligomer/polymer containing terminal hydroxyl groups which is subsequently etherified to give a polyoxyalkylene glycol of Formula I. The polyoxyalkylene glycol lubricant which is finally formed will not usually consist of a single compound of Formula I, but will usually comprise a mixture of such compounds which vary from one another in respect of the degree of polymerisation, i.e. the number of ethylene and/or propylene oxide residues. Moreover, a mixture of alcohols and/or phenols may be used as initiators in the formation of the polyoxyalkylene glycol lubricant, and a mixture of etherifying agents which provide different Q groups may also be used. The molecular weight of a polyoxyalkylene glycol lubricant comprising a mixture of compounds of Formula I will represent the average molecular weight of all the compounds present, so that a given lubricant may contain specific polyoxyalkylene glycols which have a molecular weight outside the range quoted above, providing that the

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average molecular weight of all the compounds is within that range.

The moiety A in the polyoxyalkylene glycol of Formula I is the residue remaining after removing the hydroxyl groups from a hydroxyl containing organic compound. Such compounds include the mono- and polyhydric alcohols and phenols. Where the hydroxyl containing organic compound which is used as an initiator in the formation of the polyoxyalkylene glycol is a monohydric alcohol or phenol, A is preferably a hydrocarbyl group and more preferably is an alkyl, aryl, alkaryl or aralkyl group, especially alkyl. Suitable alkyl groups for A may be selected from the straight chain (linear), branched or cyclic alkyl groups. Preferably, A is a C₁₋₁₂, particularly a C₁₋₁₀ and especially a C₁₋₆ alkyl group. Specific examples of alkyl groups include methyl, ethyl, n-propyl, isopropyl, n-butyl, isobutyl, sec-butyl, tert-butyl, the various pentyl groups, the various hexyl groups, cyclopentyl, cyclohexyl and the like. Particularly preferred alkyl groups for A are the C₁₋₁₂, particularly the C₁₋₁₀ and especially the C₁₋₆ straight chain alkyl groups, examples of which have been listed above. An especially preferred alkyl group for A is methyl or n-butyl.

Other suitable hydrocarbyl groups for A are those which remain after removing a hydroxyl group(s) from benzyl alcohol and phenols such as phenol, cresol, nonylphenol, resorcinol and bisphenol A.

Where a polyhydric alcohol is used in the formation of the polyoxyalkylene glycol, A is preferably a hydrocarbon radical. Suitable hydrocarbon radicals for A are those which remain after removing the hydroxyl groups from polyhydric alcohols such as

5 ethylene glycol, propylene glycol, 1,4-butanediol,
1,6-hexanediol, diethylene glycol, dipropylene glycol,
cyclohexane dimethanol, glycerol, 1,2,6-hexane triol,
trimethylolpropane, pentaerythritol, dipentaerythritol
and sorbitol. A particularly preferred hydrocarbon
radical for A is that remaining after removing the
hydroxyl groups from glycerol.

10 The moiety Q in the polyoxyalkylene glycol of
Formula I is an optionally substituted alkyl, aralkyl
or aryl group. A preferred optionally substituted
aralkyl group for Q is an optionally substituted benzyl
15 group. Preferred optionally substituted aryl groups for
Q include phenyl and alkyl substituted phenyl groups.
Preferably, Q is an optionally substituted, for example
halogen substituted, alkyl group, particularly an
optionally substituted C₁₋₁₂ alkyl group and more
20 particularly an optionally substituted C₁₋₄ alkyl
group. Suitable alkyl groups for Q may be selected from
the straight chain (linear), branched or cyclic alkyl
groups, especially the linear alkyl groups. Although
the alkyl groups for Q are described as being
25 optionally substituted, they are preferably
unsubstituted. Accordingly, particularly preferred
alkyl groups for Q are selected from methyl, ethyl,
propyl, isopropyl and the various butyl groups. An
especially preferred alkyl group for Q is methyl.

30 The polyoxyalkylene glycol of Formula I may be a
polyoxyethylene glycol, a polyoxypropylene glycol or a
poly(oxyethylene/oxypropylene) glycol. In the latter
case, the ethylene and propylene oxide residues may be
arranged randomly or in blocks along the polymer chain.
Preferred polyoxyalkylene glycols are the
35 polyoxypropylene glycols and the
poly(oxyethylene/oxypropylene) glycols.

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5 Particularly preferred lubricants for use in the
working fluid compositions of the invention are those
selected from the class known as neopentyl polyol
esters due, inter alia, to their generally high level
of thermal stability. Suitable neopentyl polyol esters
include the esters of pentaerythritol,
10 polypentaerythritols such as di- and
tripentaerythritol, trimethylol alkanes such as
trimethylol ethane and trimethylol propane, and
neopentyl glycol. Such esters may be formed with linear
and/or branched aliphatic carboxylic acids, such as
15 linear and/or branched alkanolic acids, or esterifiable
derivatives thereof. A minor proportion of an aliphatic
polycarboxylic acid, e.g. an aliphatic dicarboxylic
acid, or an esterifiable derivative thereof may also be
used in the synthesis of the ester lubricant in order
20 to increase the viscosity thereof. However, where such
an aliphatic polycarboxylic acid (or esterifiable
derivative thereof) is employed in the synthesis, it
will preferably constitute no more than 30 mole %, more
preferably no more than 10 mole % of the total amount
25 of carboxylic acids (or esterifiable derivatives
thereof) used in the synthesis. Usually, the amount of
the carboxylic acid(s) (or esterifiable derivative
thereof) which is used in the synthesis will be
sufficient to esterify all of the hydroxyl groups
30 contained in the polyol, but in certain circumstances
residual hydroxyl functionality may be acceptable.

A preferred neopentyl polyol ester lubricant is
one comprising one or more compounds of general
formula:



wherein

5 R is the hydrocarbon radical remaining after removing the hydroxyl groups from pentaerythritol, dipentaerythritol, tripentaerythritol, trimethylol ethane, trimethylol propane or neopentyl glycol, or the hydroxyl containing hydrocarbon radical remaining after removing a proportion of the hydroxyl groups from
10 pentaerythritol, dipentaerythritol, tripentaerythritol, trimethylol ethane, trimethylol propane or neopentyl glycol;

each R^1 is, independently, H, a straight chain (linear) aliphatic hydrocarbyl group, a branched
15 aliphatic hydrocarbyl group, or an aliphatic hydrocarbyl group (linear or branched) containing a carboxylic acid or carboxylic acid ester substituent, provided that at least one R^1 group is a linear aliphatic hydrocarbyl group or a branched aliphatic
20 hydrocarbyl group; and

n is an integer.

The aliphatic hydrocarbyl groups specified for R^1 above may be substituted, e.g. by pendant atoms or groups such as chloro, fluoro and bromo, and/or by in
25 chain hetero atoms such as oxygen and nitrogen. Preferably, however, such hydrocarbyl groups are unsubstituted and, except in the case where R^1 is an aliphatic hydrocarbyl group containing a carboxylic acid or carboxylic acid ester substituent, contain only
30 carbon and hydrogen atoms.

The ester lubricants of Formula II may be prepared by reacting the appropriate polyol or mixture of polyols with the appropriate carboxylic acid or mixture of acids. Esterifiable derivatives of the carboxylic
35 acids may also be used in the synthesis, such as the acyl halides, anhydrides and lower alkyl esters

thereof. Suitable acyl halides are the acyl chlorides and suitable lower alkyl esters are the methyl esters. Aliphatic polycarboxylic acids, or esterifiable derivatives thereof, may also be used in the synthesis of the ester lubricant. Where an aliphatic polycarboxylic acid is used in the synthesis of the ester lubricant, the resulting lubricant will comprise one or more compounds of Formula II in which at least one of the R^1 groups is an aliphatic hydrocarbyl group (linear or branched) containing a carboxylic acid or carboxylic acid ester substituent. The ability of polycarboxylic acids to react with two or more alcohol molecules provides a means of increasing the molecular weight of the ester formed and so a means of increasing the viscosity of the lubricant. Examples of such polycarboxylic acids include maleic acid, adipic acid and succinic acid, especially adipic acid. Generally, however, only monocarboxylic acids (or esterifiable derivatives thereof) will be used in the synthesis of the ester lubricant, and where polycarboxylic acids are used they will be used together with one or more monocarboxylic acids (or esterifiable derivatives thereof) and will constitute only a minor proportion of the total amount of carboxylic acids used in the synthesis. Where an aliphatic polycarboxylic acid (or an esterifiable derivative thereof) is employed in the synthesis, it will preferably constitute no more than 30 mole %, more preferably no more than 10 mole % of the total amount of carboxylic acids used in the synthesis, with one or more monocarboxylic acids (or esterifiable derivatives thereof) constituting the remainder.

Usually, the amount of the carboxylic acid(s) (or esterifiable derivative thereof) which is used in the

5 synthesis will be sufficient to esterify all of the
hydroxyl groups contained in the polyol(s), in which
case the resulting lubricant will comprise one or more
compounds of Formula II in which R is the hydrocarbon
radical remaining after removing the hydroxyl groups
from pentaerythritol, dipentaerythritol,
tripentaerythritol, trimethylol ethane, trimethylol
10 propane or neopentyl glycol. However, in certain
circumstances ester lubricants which comprise residual
hydroxyl functionality may be acceptable. Such
lubricants comprise one or more ester compounds of
Formula II in which R is the hydroxyl containing
15 hydrocarbon radical remaining after removing a
proportion of the hydroxyl groups from pentaerythritol,
dipentaerythritol, tripentaerythritol, trimethylol
ethane, trimethylol propane or neopentyl glycol. Esters
containing residual (unreacted) hydroxyl functionality
20 are often termed partial esters, and lubricants
containing them may be prepared by utilising an amount
of the carboxylic acid or acids which is insufficient
to esterify all of the hydroxyl groups contained in the
polyol or polyols.

25 It will be appreciated that the preferred
neopentyl polyol ester lubricants may comprise a single
compound of Formula II, i.e. the reaction product which
is formed between a single polyol and a single
monocarboxylic acid. However, such ester lubricants may
30 also comprise a mixed ester composition comprising two
or more compounds of Formula II. Such mixed ester
compositions may be prepared by utilising two or more
polyols and/or two or more carboxylic acids (or
esterifiable derivatives thereof) in the synthesis of
35 the ester, or by combining a mixture of different
esters each of which is the reaction product of a

particular polyol and a particular carboxylic acid.
Furthermore, different mixed ester compositions, each
of which has been prepared by utilising two or more
polyols and/or two or more carboxylic acids (or
esterifiable derivatives thereof) in their synthesis,
may also be blended together.

The preferred neopentyl polyol ester lubricants
comprise one or more compounds of Formula II in which R
is the hydrocarbon radical remaining after removing the
hydroxyl groups from pentaerythritol,
dipentaerythritol, trimethylol propane or neopentyl
glycol. Particularly preferred alcohols for the
synthesis of the ester are pentaerythritol,
dipentaerythritol and trimethylol propane.

Preferably, each R¹ in Formula II is,
independently, a linear aliphatic hydrocarbyl group or
a branched aliphatic hydrocarbyl group.

Preferred linear aliphatic hydrocarbyl groups for
R¹ are the linear alkyl groups, particularly the C₃₋₁₀
linear alkyl groups, more particularly the C₅₋₁₀ linear
alkyl groups and especially the C₅₋₈ linear alkyl
groups. Examples of suitable linear alkyl groups
include n-pentyl, n-hexyl, n-heptyl, n-octyl, n-nonyl
and n-decyl. Esters containing such alkyl groups can be
prepared by utilising a linear alkanolic acid in the
synthesis of the ester.

Preferred branched aliphatic hydrocarbyl groups
for R¹ are the branched alkyl groups, particularly the
C₄₋₁₄ branched alkyl groups, more particularly the
C₆₋₁₂ branched alkyl groups and especially the C₈₋₁₀
branched alkyl groups. Examples of suitable branched
alkyl groups include isopentyl, isohexyl, isoheptyl,
isooctyl, isononyl, isodecyl, 2-ethylbutyl,
2-methylhexyl, 2-ethylhexyl, 3,5,5-trimethylhexyl,

neopentyl, neoheptyl and neodecyl. Esters containing such alkyl groups can be prepared by utilising a branched alkanoic acid in the synthesis of the ester.

In a particularly preferred embodiment of the present invention, the ester lubricant comprises one or more esters of general formula:



wherein

15 R^2 is the hydrocarbon radical remaining after removing the hydroxyl groups from pentaerythritol, dipentaerythritol or trimethylol propane;

each R^3 is, independently, a linear alkyl group or a branched alkyl group; and

20 p is an integer of 3, 4 or 6,
wherein one or more of the named polyols, one or more linear alkanoic acids, or esterifiable derivatives thereof, and optionally one or more branched alkanoic acids, or esterifiable derivatives thereof, are
25 utilised in the synthesis of the ester lubricant.

Preferably, a mixture of two or more linear alkanoic acids, in particular two, or esterifiable derivatives thereof, are utilised in the synthesis of the ester. More preferably, a mixture of one or more
30 linear alkanoic acids, or esterifiable derivatives thereof, and one or more branched alkanoic acids, or esterifiable derivatives thereof, are utilised in the synthesis. Thus, particularly preferred ester
lubricants of the invention are mixed ester
35 compositions which comprise a plurality of compounds of Formula III.

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Where a mixture of linear and branched alkanolic acids (or esterifiable derivatives thereof) are
5 utilised in the synthesis of the ester, as is preferred, the linear alkanolic acid(s) preferably constitutes at least 25 mole %, e.g. from 25 to 75 mole %, of the total amount of carboxylic acids used. In this way, at least 25 mole %, e.g. from 25 to 75
10 mole %, of the hydroxyl groups contained in the polyol or mixture of polyols may be reacted with the said linear alkanolic acid(s).

Ester based lubricants comprising one or more compounds of Formula III provide a particularly good
15 balance between the properties desired of a lubricant and, in particular, exhibit good thermal stability, good hydrolytic stability and acceptable solubility and miscibility with the heat transfer fluid. As stated previously, the present invention is particularly
20 concerned with the provision of a working fluid composition which can replace the existing working fluid compositions comprising R-22 or R-502 as the refrigerant. Refrigeration systems which contain replacements for R-22 and R-502 typically operate at
25 temperatures above those using R-134a as the sole replacement refrigerant. Thus, it is particularly desirable that the lubricant which is used in a working fluid composition designed to replace the existing compositions based on R-22 and R-502 exhibits good
30 thermal stability.

Preferably, R^2 is the hydrocarbon radical remaining after removing the hydroxyl groups from pentaerythritol or dipentaerythritol.

Preferred linear and branched alkyl groups for R^3
35 are those described above in connection with R^1 and are

derived by utilising the corresponding alkanolic acids or esterifiable derivatives thereof.

5 An especially preferred ester based lubricant comprises a mixed ester composition which comprises a plurality of esters of Formula III and which is the reaction product of pentaerythritol, heptanoic acid and a mixture of branched C₈-10 alkanolic acids. Preferably, 10 the heptanoic acid will constitute from 25 to 75 mole % of the total amount of acids utilised in the synthesis, with the branched C₈-10 acids constituting the remainder. Esterifiable derivatives of the acids may also be used in the synthesis of the ester.

15 The lubricant will typically be part of a lubricant composition which also comprises one or more of the additives which are conventional in the refrigeration lubricants art. Specific mention may be made of oxidation resistance and thermal stability 20 improvers, corrosion inhibitors, metal deactivators, viscosity index improvers, anti-wear agents and extreme pressure resistance additives. Such additives are well known to those skilled in the art. Where the lubricant is part of a lubricant composition containing one or 25 more additives, such additives may be present in the amounts conventional in the art. Preferably, the cumulative weight of all the additives will not be more than 8 %, e.g. 5 %, of the total weight of the lubricant composition.

30 Suitable oxidation resistance and thermal stability improvers may be selected from the diphenyl-, dinaphthyl-, and phenylnaphthyl-amines, the phenyl and naphthyl groups of which may be substituted. Specific examples include N,N'-diphenyl phenylenediamine, 35 p-octyldiphenylamine, p,p-dioctyldiphenylamine, N-phenyl-1-naphthyl amine, N-phenyl-2-naphthyl amine,

5 N-(p-dodecyl)-phenyl-2-naphthyl amine, di-1-naphthyl
amine, and di-2-naphthyl amine. Other suitable
oxidation resistance and thermal stability improvers
may be selected from the phenothiazines such as
N-alkylphenothiazines, and the hindered phenols such as
6-(t-butyl) phenol, 2,6-di-(t-butyl) phenol,
4-methyl-2,6-di-(t-butyl) phenol and
10 4,4'-methylenebis(-2,6-di-[t-butyl] phenol).

Suitable cuprous metal deactivators may be
selected from imidazole, benzimidazole,
2-mercaptobenzthiazole, 2,5-dimercaptothiadiazole,
salicylidine-propylenediamine, pyrazole, benzotriazole,
15 tolutriazole, 2-methylbenzimidazole, 3,5-dimethyl
pyrazole, and methylene bis-benzotriazole. Examples of
more general metal deactivators and/or corrosion
inhibitors include organic acids and the esters, metal
salts and anhydrides thereof, such as
20 N-oley- sarcosine, sorbitan monooleate, lead
naphthenate, dodecenyl-succinic acid and its partial
esters and amides, and 4-nonylphenoxy acetic acid;
primary, secondary and tertiary aliphatic and
cycloaliphatic amines and amine salts of organic and
25 inorganic acids, such as oil soluble alkylammonium
carboxylates; heterocyclic nitrogen containing
compounds, such as thiadiazoles, substituted
imidazolines, and oxazolines; quinolines, quinones and
anthraquinones; ester and amide derivatives of alkenyl
30 succinic anhydrides or acids, dithiocarbamates,
dithiophosphates; and amine salts of alkyl acid
phosphates and their derivatives.

Suitable viscosity index improvers include
polymethacrylate polymers, copolymers of vinyl
pyrrolidone and methacrylates, polybutene polymers, and
35 copolymers of styrene and acrylates.

5 Examples of suitable anti-wear and extreme
pressure resistance agents include sulphurised fatty
acids and fatty acid esters, such as sulphurised octyl
tallate; sulphurised terpenes; sulphurised olefins;
organopolysulphides; organo phosphorous derivatives
including amine phosphates, alkyl acid phosphates,
10 dialkyl phosphates, aminedithiophosphates, trialkyl and
triaryl phosphorothionates, trialkyl and triaryl
phosphines, and dialkylphosphites, e.g., amine salts of
phosphoric acid monohexyl ester, amine salts of
dinonylnaphthalene sulphonate, triphenyl phosphate,
15 trinaphthyl phosphate, diphenyl cresyl and dicresyl
phenyl phosphates, tricresyl phosphate, naphthyl
diphenyl phosphate, triphenylphosphorothionate;
dithiocarbamates, such as an antimony dialkyl
dithiocarbamate; chlorinated and/or fluorinated
hydrocarbons, and xanthates.

20 The working fluid compositions of the invention
will typically comprise a major amount of the heat
transfer fluid and a minor amount of the synthetic
lubricant. Preferably, the working fluid compositions
of the invention will comprise from 50 to 99 % by
25 weight, more preferably from 70 to 99 % by weight, of
the heat transfer fluid and from 1 to 50 % by weight,
more preferably from 1 to 30 % by weight, of the
lubricant based on the total weight thereof.

30 The working fluid compositions are useful in all
types of compression cycle heat transfer devices. Thus,
they may be used to provide cooling by a method
involving condensing the heat transfer fluid and
thereafter evaporating it in a heat exchange
relationship with a body to be cooled. They may also
35 be used to provide heating by a method involving
condensing the heat transfer fluid in a heat exchange

relationship with a body to be heated and thereafter evaporating it.

5 The working fluid compositions of the invention provide a good compromise between performance and low or zero ozone depletion. They are especially suitable for applications currently satisfied by refrigerants R-22 and R-502.

10 The present invention is now illustrated, but not limited, with reference to the following Examples.

 The working fluid compositions of the invention which were investigated in the following Examples comprised a lubricant and a heat transfer fluid which
15 was either a binary mixture of 1,1,1,2-tetrafluoroethane (R-134a) and difluoromethane (R-32) or a ternary mixture of 1,1,1,2-tetrafluoroethane (R-134a), difluoromethane (R-32) and pentafluoroethane (R-125).

 1,1,1,2-tetrafluoroethane, difluoromethane and
20 pentafluoroethane are at least partially soluble in each of the lubricants tested which means the converse is true, i.e. each of the lubricants tested will be at least partially soluble in each of these hydrofluoroalkanes. Moreover, each lubricant tested is
25 at least partially soluble in the binary or ternary mixtures themselves.

Example 1

30 In this Example various working fluid compositions were prepared comprising 15 % w/w of a lubricant and the complementary percentage of a heat transfer fluid comprising (by weight) equal proportions of R-134a and R-32. The lower miscibility temperature of each
35 composition, i.e. the lowest temperature at which the lubricant remained miscible with the heat transfer

fluid, was determined. The method employed was as follows:

5 A set amount of the lubricant to be tested was placed in a previously evacuated thick walled test tube and the tube was then placed in a cooling bath regulated at the desired temperature. Once the tube was sufficiently cold, a set amount of the heat transfer
10 fluid was condensed into the test tube. The tube was then removed from the cooling bath and the contents allowed to warm to room temperature. After the contents had been allowed to equilibrate at room temperature, they were agitated and visually examined for evidence
15 of phase separation (the mixture looks cloudy). If there was no evidence of phase separation, the temperature of the mixture was lowered in a cooling bath at a rate of 1 °C per minute until phase separation was observed. The temperature at which phase
20 separation was first observed was recorded as the lower miscibility temperature.

 The results are shown in Table 1. Each lubricant is at least partially soluble in each of the components of the heat transfer fluid and also in the fluid
25 itself.

 The lower miscibility temperatures of a series of compositions comprising 15 % w/w of a lubricant and the complementary percentage of a single hydrofluoroalkane selected from R-134a, R-32 and R-125 were also
30 determined. The compositions were prepared and the lower miscibility temperatures determined using the procedure described above. The results are shown in Table 1A. In Table 1A it will be noticed that the lower miscibility temperatures are in some cases quoted as
35 being less than -60 °C. This means that at -60 °C phase separation was not observed.

TABLE 1

LUBRICANT	LOWER MISCIBILITY TEMPERATURE (°C)
PE6	-27
"EMKARATE" (TM) RL-212	-3
"EMKARATE" (TM) RL-184	>10
"EMKAROX" (TM) RL-118	I

TABLE 1A

LUBRICANT	LOWER MISCIBILITY TEMPERATURE (°C)		
	R-134a	R-32	R-125
PE6	<-60	0	<-60
"EMKARATE" (TM) RL-212	-25	>20	<-60
"EMKARATE" (TM) RL-184	10	>20	<-60
"EMKAROX" (TM) RL-118	<-60	I	<-60

I - denotes immiscibility over the temperature range -50 °C to +20 °C.

PE6 is an ester of pentaerythritol and n-hexanoic acid.

"EMKARATE" (TM) RL-212 is a commercially available ester based lubricant for use with R-134a obtainable from ICI Chemicals & Polymers Ltd. Specifically, the lubricant comprises an ester of trimethylol propane and heptanoic acid.

"EMKARATE" (TM) RL-184 is a commercially available ester based lubricant for use with R-134a obtainable from ICI Chemicals & Polymers Ltd. Specifically, the

lubricant comprises an ester of pentaerythritol,
heptanoic acid and a mixture of branched C₈₋₁₀ alkanolic
acids.

"EMKAROX" (TM) RL-118 is a commercially available
polyoxyalkylene glycol based lubricant for use with
R-134a obtainable from ICI Chemicals & Polymers Ltd.
Specifically, the lubricant comprises an end-capped
polyoxyalkylene glycol.

"EMKARATE" and "EMKAROX" are trademarks of ICI
Chemicals & Polymers Ltd.

Example 2

In this Example a series of working fluid
compositions were prepared comprising varying
proportions of a lubricant comprising an ester of
pentaerythritol and n-hexanoic acid and a heat transfer
fluid comprising 70 % by weight of R-134a and 30 % by
weight of R-32. The lubricant is at least partially
soluble in each of the components of the heat transfer
fluid and also in the fluid itself. The lower
miscibility temperature of each composition was
determined. The compositions were prepared and the
lower miscibility temperatures determined using the
procedure described in Example 1.

The results are shown in Table 2. In Table 2 it
will be noticed that the lower miscibility temperature
of one of the compositions is quoted as being less than
-50 °C. This means that at -50 °C phase separation was
not observed.

TABLE 2

Working fluid composition		Lower miscibility temperature (°C)
% by weight of lubricant	% by weight of heat transfer fluid	
10.8	89.2	-30
20.3	79.7	-25
27.5	72.5	-32
36.9	63.1	-38
46.0	54.0	-47
68.0	32.0	< -50

Example 3

In this Example a series of working fluid compositions were prepared comprising varying proportions of a lubricant and a heat transfer fluid comprising 70 % by weight of R-134a and 30 % by weight of R-32. The lubricant comprised an ester of dipentaerythritol, n-hexanoic acid and a branched C₆ carboxylic acid, i.e. a branched acid comprising 6 carbon atoms, and is at least partially soluble in each of the components of the heat transfer fluid and also in the fluid itself. The lower miscibility temperature of each composition was again determined. The compositions were prepared and the lower miscibility temperatures determined using the procedure described in Example 1.

The results are shown in Table 3. In Table 3 it will be noticed that the lower miscibility temperature of one of the compositions is quoted as being less than

-55 °C. This means that at -55 °C phase separation was not observed.

TABLE 3

Working fluid composition		Lower miscibility temperature (°C)
% by weight of lubricant	% by weight of heat transfer fluid	
10.0	90.0	-32
17.3	82.7	-28
38.0	62.0	-35
46.2	53.8	-41
57.8	42.2	Slightly immiscible at -55
68.8	31.2	< -55

Example 4

In this Example a series of working fluid compositions were prepared comprising varying proportions of a lubricant and a heat transfer fluid comprising 70 % by weight of R-134a and 30 % by weight of R-32. The lubricant comprised a mixture of the lubricants used in Examples 2 and 3, i.e. a mixture comprising an ester of pentaerythritol and n-hexanoic acid and an ester of dipentaerythritol, n-hexanoic acid and a branched C₆ carboxylic acid, and is at least partially soluble in each of the components of the heat transfer fluid and also in the fluid itself. The lower miscibility temperature of each composition was again determined. The compositions were prepared and the

lower miscibility temperatures determined using the procedure described in Example 1.

The results are shown in Table 4. In Table 4 it will be noticed that the lower miscibility temperature of one of the compositions is quoted as being less than -50 °C. This means that at -50 °C phase separation was not observed.

TABLE 4

Working fluid composition		Lower miscibility temperature (°C)
% by weight of lubricant	% by weight of heat transfer fluid	
10.5	89.5	-31
19.7	80.3	-27
28.9	71.1	-29
41.1	58.9	-32
48.0	52.0	-39
55.2	44.8	-46
69.7	30.3	< -50

Example 5

In this Example a series of working fluid compositions were prepared comprising varying proportions of a lubricant comprising an ester of pentaerythritol and n-hexanoic acid and a heat transfer fluid comprising 50 % by weight of R-134a, 30 % by weight of R-32 and 20 % by weight of R-125. The lubricant is at least partially soluble in each of the components of the heat transfer fluid and also in the fluid itself. The lower miscibility temperature of each composition was again determined. The compositions were

prepared and the lower miscibility temperatures determined using the procedure described in Example 1.

The results are shown in Table 5. In Table 5 it will be noticed that the lower miscibility temperature of some of the compositions is quoted as being less than -50 °C. This means that at -50 °C phase separation was not observed.

TABLE 5

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Working fluid composition		Lower miscibility temperature (°C)
Z by weight of lubricant	Z by weight of heat transfer fluid	
10.2	89.8	< -50
22.0	78.0	-48
29.7	70.3	< -50
41.6	58.4	< -50
48.6	51.4	< -50
60.7	39.3	< -50

It will be appreciated that the binary mixtures of R-134a and R-32 and the ternary mixtures of R-134a, R-32 and R-125 which form the subject of the above Examples can also be used in combination with other neopentyl polyol ester type lubricants to yield viable working fluid compositions. Moreover, binary mixtures of R-134a and R-32 and ternary mixtures of R-134a, R-32 and R-125 comprising different proportions of the constituent hydrofluoroalkanes to the mixtures exemplified above can also be used in combination with neopentyl polyol ester type lubricants to yield viable working fluid compositions.